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# **EUROPEAN PATENT APPLICATION**

⑰ Application number: 80100310.4

⑤① Int. Cl.<sup>3</sup>: **G 02 B 5/14**

⑳ Date of filing: 22.01.80

③⑥ Priority: 22.01.79 US 5616

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④③ Date of publication of application: 06.08.80  
Bulletin 80/16

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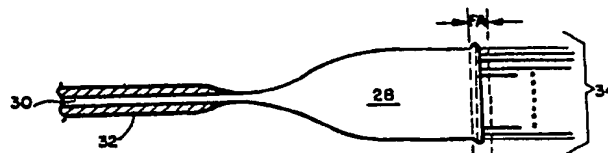
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⑤④ **Tapered mixing rod for a fiber optical multi-port coupler.**

⑤⑦ An apparatus for improved efficiency coupling of optical energy is disclosed. Coupling of the optical energy from one or more input fiber optic cables (30, 32) to a larger number of output fiber optic cables (34) is accomplished by means of a mixing rod (28) having input and output cross-sectional areas substantially matched to the input and output coupled fiber groups, respectively, and having appropriate tapering of the rod crosssection therebetween.

As a result of tapering the mixing rod, the coupler provides gradual reflection angle reduction that permits retention of the transmission system numerical aperture despite random refractive bending due to surface imperfections at the mixing rod/fiber coupling junction. In addition, an input coupling junction of prior art straight mixing rod couplers is obviated in the tapered mixing rod coupler, thereby eliminating a source of undesirable coupling loss.



**EP 0 013 972 A1**

BACKGROUND OF THE INVENTION

## 1. Field of the Invention.

This invention relates generally to the art of fiber optic transmission lines and more specifically to a novel means for coupling the light energy from one or more fiber optic cables to a larger number of fiber optic cables, but with improved operating efficiency and reduced energy losses as compared to prior art fiber optic couplers.

## 2. Description of the Prior Art.

The use of couplers, also known as power splitters, is well known in a large number of energy transmission systems. For example, waveguide and coaxial couplers are well known in the microwave communications industry as a means of splitting the power available at one point in the communications line into a selected number of multiple power levels for transmission to a plurality of terminal ports. With the relatively recent advent of fiber optic communications systems for a variety of purposes including telephone communications, and other communication systems with broad bandwidth and insensitivity to electromagnetic interference, a need has arisen for means for coupling or splitting the transmitted light energy just as that need exists in the microwave communications field. In both the microwave and optical power transmission systems, the process of coupling the energy from at least one input line to a larger number of output lines, results in a reduction in the coupled energy available at each output line. This energy reduction is due to two different phenomena. One such phenomenon is the inherent energy reduction due to the ratio of division between the number of input lines, usually one, and the larger number of output lines.

2  
1 As long as the coupler is a passive device and not a more  
2 costly active coupler that utilizes amplification, the coupling  
3 loss, per se, is unavoidable and is usually designed into the  
4 system so that the power level in the output-coupled ports is  
5 still sufficient to serve the minimum power requirements of  
6 the system. However, coupling loss also occurs as a result  
7 of inadvertent reflections at the coupling junctions, the  
8 inadvertent conversion of the energy into other forms of energy  
9 that are not useable in the system, and other similar phenomena  
10 that produce inadvertent losses that the designer attempts  
11 to reduce to a minimum in order to provide a coupling  
12 efficiency that is as high as possible.

13  
14 In the fiber optics art there are a number of well known  
15 means for coupling light energy from one or more input fibers  
16 to a larger number of output fibers. One such coupler of the  
17 prior art is known as a mixing rod coupler in which a rod,  
18 usually made of the same material as that of the fiber and  
19 having a cross-sectional diameter equal to the group of output  
20 fibers, is utilized as a means of dispersing the input light  
21 energy from at least one fiber to a plurality of output fibers  
22 in roughly equal energy levels. The term "mixing" is applied  
23 to such a rod, because when the mixing rod is used with more  
24 than one input fiber cable, the signals on the respective  
25 input cables are mixed in the rod before being applied to the  
26 output cables. Accordingly, the term "mixing" is somewhat  
27 of a misnomer with respect to a coupler that has only one  
28 input fiber. However, it has become more or less a standard  
29 term in the art and is used herein to apply to both the single  
30 and multiple input fiber cases.

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Mixing rod couplers of the prior art introduce a number of the aforementioned inadvertent coupling losses which are preferably avoided, if possible, so that the power levels of the signals coupled to the output cables more closely approach the ideal power levels resulting only from the ratio of the number of input lines to the number of output lines. Such inadvertent coupling losses in prior art couplers result from both the losses inherent in each coupling junction between the coupling assembly and the input and output fibers and also from the inefficiency of the optical geometry of such prior art couplers. The geometrical inefficiency of prior art mixing rod couplers results primarily from the use of a cross-sectional area which remains constant throughout the length of the rod. Thus, although output cross section of the prior art mixing rod is optimized for coupling to the output fiber group, the input cross section of the mixing rod is far less than optimum for coupling to the input fiber or fiber group. Accordingly, the purpose of the present invention is to substantially reduce the inadvertent coupling losses of prior art mixing rod couplers by reducing the number of coupling junctions in the coupling assembly interfaced with the input fiber group and also by utilizing a geometrical configuration that is optimized for both the input and output group of fibers.

#### SUMMARY OF THE INVENTION

The present invention is a mixing rod coupler in which the constant cross section mixing rod of the prior art is replaced by a mixing rod that is tapered so that its cross section is substantially matched to both the input and output fiber groups. The resulting coupler obviates the inherent area mismatch of

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1 prior art mixing rod couplers and also reduces the number of  
2 coupling joints of prior art mixing rod couplers. In addition,  
3 the novel geometry of the present invention permits retention  
4 of the numerical aperture of the input fiber optic cable that  
5 is otherwise reduced in prior art couplers due to inadvertent  
6 random refractive bending that usually occurs due to imperfect  
7 surfaces at the output coupling junction. The invention is  
8 therefore, an improved mixing rod coupler in which inadvertent  
9 coupling losses, that is, losses other than those due to the  
10 coupling ratio, are substantially reduced as compared to  
11 conventional straight mixing rod couplers of the prior art.

12  
13 The aforementioned disadvantages of the prior art and the  
14 manner in which the novel geometrical configuration of the  
15 present invention substantially reduces the inadvertent coupling  
16 losses resulting from those prior art disadvantages, will  
17 be better understood from the detailed description of the  
18 invention to follow, taken in conjunction with the accompanying  
19 drawings in which:

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BRIEF DESCRIPTION OF THE DRAWINGS

1  
2  
3 Fig. 1 is an illustrative drawing of a multi-port coupler  
4 assembly that employs a straight mixing rod of the prior art;

5  
6 Fig. 2 is a conceptual illustration of the manner in which an  
7 optical signal is coupled in a prior art multi-port coupler  
8 employing a straight mixing rod;

9  
10 Fig. 3 is a conceptual illustration used to explain a  
11 significant disadvantage of straight mixing rod couplers that  
12 is substantially overcome by means of the present invention;

13  
14 Fig. 4 is a conceptual illustration of the manner in which  
15 an optical signal is coupled by means of the present invention;

16  
17 Fig. 5 is an illustrative drawing used to explain the manner  
18 in which the advantageous coupling characteristics of the  
19 present invention are achieved; and.

20  
21 Fig. 6 provides an illustrative example of the manner in  
22 which an embodiment of the present invention, suitable for  
23 coupling a single input fiber to a group of output fibers,  
24 may be manufactured.

25  
26 DETAILED DESCRIPTION OF THE INVENTION

27  
28 Simply stated, a mixing rod coupler couples the optical output  
29 signal of a single fiber or a group of fibers to the input  
30 ports of another, usually larger, group of fibers. Fig. 1  
31 illustrates the operation of one such coupler that employs a  
32

1 prior art straight mixing rod. Prior art coupler 10 couples  
2 the output signal of a single input fiber 13 to a group of  
3 output fibers 14. In other words, light transmission is from  
4 left to right in Fig. 1. In addition to the straight mixing  
5 rod 16, the coupler also includes a fabrication collar 18  
6 and a suitable optical epoxy 20 which holds the input and  
7 output fibers in their respective positions with respect to  
8 coupler 10. The optical coupling, per se, is achieved by the  
9 straight mixing rod 16. The purpose of the collar 18 is  
10 twofold, namely, that of holding the fibers in a close-packed  
11 parallel alignment against the mixing rod face and also of  
12 providing a protective encapsulation for the finished coupler.  
13 It is interesting to note that in the prior art coupler  
14 of Fig. 1, the protective collar is tapered to provide improved  
15 alignment of the single input fiber 13 with respect to the  
16 input face of mixing rod 16. However, the mixing rod itself  
17 is straight in that it has substantially parallel straight  
18 edges along the longitudinal axis of coupler 10. These straight  
19 parallel edges provide optical signal reflections as illustrated  
20 conceptually in Fig. 2.

21  
22 As indicated in Fig. 2, a typical straight mixing rod coupler  
23 assembly comprises the mixing rod 16, an input interface fiber  
24 13, and output interface fibers 14. As a result, a first  
25 coupling junction C1 exists at the interface between fiber 13  
26 and the system input fiber 12; a second coupling junction A1  
27 exists at the interface between the fiber 13 and the mixing  
28 rod 16; a third coupling junction B1 exists at the interface  
29 of mixing rod 16 and fibers 14, and a fourth coupling junction  
30 D1 exists at the interface between fibers 14 and system output  
31 fibers 15.

32



1       As shown in Fig. 2, light enters the coupling assembly 10  
2       through the input interface fiber 13 at the left-most portion  
3       of the coupler at coupler junction C1. As is well known in the  
4       fiber optic art, the light entering the fiber at an angle with  
5       respect to the longitudinal axis of the fiber, experiences  
6       multiple reflections at the fiber edge or cladding as it passes  
7       along the core of the fiber. In the case of a straight mixing  
8       rod, the angle of reflection is maintained through the input  
9       interface fiber 13, the mixing rod 16 and ultimately, the  
10      output interface fibers 14 beyond coupler junction B1. Because  
11      of the straight, parallel edges in mixing rod 16, the angle  
12      of reflection of the light energy with respect to the edge  
13      of the mixing rod, is maintained as a constant angle of  
14      reflection  $\theta_f$  which is typically equal to about 10 degrees.

15  
16      It is well known that optical fibers are designed with a  
17      particular maximum angle with respect to the center line of  
18      the fiber at which light rays may enter the fiber and be  
19      transferred along the length of the fiber. In a typical  
20      fiber, this maximum angle might be, by way of example, 10  
21      degrees, in which case, no light rays can be transmitted in  
22      the fiber at an angle  $\theta_f$  greater than 10 degrees. Any light  
23      ray which enters the fiber with an angle greater than this  
24      maximum value is lost through the cladding of the fiber by  
25      mechanisms which are well known in the art of fiber optics.  
26      Thus, this maximum angle is a limit of the angle with respect  
27      to the center line of the fiber at which the fiber can accept  
28      incoming light and transfer that light with minimum attenuation.  
29      The sine of this maximum angle multiplied by the index of  
30      refraction of the fiber material, is equal to the numerical  
31      aperture, an important operating parameter of fiber optic

1 transmission systems. All of the light which is transmitted  
2 in the fiber must be contained within the angles between  $\theta$   
3 degrees and the maximum angle related to the numerical aperture  
4 of the fiber.

5  
6 In any optical fiber coupler device, the maximum angle is of  
7 great importance. The importance of this angle as it pertains  
8 specifically to couplers becomes clear with reference to  
9 Fig. 3. Fig. 3 represents the junction between any mixing  
10 rod MR and an output fiber OF. It is well known that in no  
11 case can the surfaces of the mixing rod MR and output fiber  
12 OF, at joint B1, be absolutely flat and perpendicular to the  
13 axis of light transmission. This lack of perfect flatness  
14 and perpendicularity is exaggerated in Fig. 3 for purposes  
15 of discussion. If a light ray exits mixing rod MR at an angle  
16  $\theta_f$ , it passes out of the mixing rod surface at point A through  
17 a separating region which may be filled with a contacting  
18 material such as optical cement, a contacting liquid, or fusing  
19 material. In any case, due to the inevitable lack of perfect  
20 index matching between the materials of the mixing rod, the  
21 contacting material and the output fiber, there is some  
22 refraction at the surface point A and further refraction at  
23 the surface point B. Because these surfaces, although they  
24 may be generally acceptable, are still not perfect and because  
25 these imperfections have random characteristics, the angle  
26 of exit of the light ray beyond surface point B may be either  
27 larger or smaller than the maximum angle  $\theta_f$ . This exit angle  
28 is denoted  $\theta_{f2}$  in Fig. 3.

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1 If  $\theta_f$  is close to, or equal to the maximum angle as previously  
2 defined,  $\theta_{f2}$  may be greater than the maximum angle  $\theta_f$ .  
3 Accordingly, when the light reaches the interface surface  
4 between the core of the output fiber and the cladding of the  
5 output fiber at surface point C, the light will be lost from  
6 the core and refracted into the cladding. This light will  
7 eventually reach the outer edge of the cladding at surface  
8 point D and much of it will be lost by dispersion and various  
9 other mechanisms. Light which is reflected back at point D  
10 towards the fiber is reflected into the cladding, remains in a  
11 cladding mode and is usually lost at other points along the  
12 outside cladding surface. Accordingly, instead of having the  
13 light that exits the mixing rod at an angle  $\theta_f$  passing into  
14 the output fiber along the dotted line to point E at the outer  
15 surface of the fiber core at the cladding interface and  
16 thereafter behaving in the assumed fashion as previously  
17 illustrated in Fig. 2, the light is bent because of imperfections  
18 in the joint between the output fiber OF and the mixing rod MR  
19 and much of the light which is bent is lost from the fibers.  
20

21 As a result, the attenuation of the coupler to light energy  
22 entering at or near the maximum angle is increased. The result  
23 is, a substantial reduction in the useable numerical aperture  
24 of the fiber transmission system that employs prior art  
25 couplers utilizing straight mixing rods. On the other hand, in  
26 the present invention the disadvantageous reduction in useable  
27 numerical aperture resulting from coupling is substantially  
28 overcome. The means by which this is accomplished in the  
29 present invention will now be discussed in conjunction with  
30 Figs. 4, 5 and 6.  
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1 As illustrated in Fig. 4, in the present invention and the  
2 straight mixing rod of the prior art is replaced by a tapered  
3 mixing rod in which the edges are substantially parallel  
4 towards the input and output coupling points, but which are  
5 tapered therebetween. This tapering characteristic substantially  
6 reduces the angle of the incoming light ray at coupling point  
7 C2 from  $\theta_f$  to  $\alpha_f$  for the light ray exiting the mixing rod  
8 at coupling point B2. Thus, in contrast to the prior art  
9 straight mixing rod, in the tapered mixing rod of the present  
10 invention, the angle which the light ray makes with the center  
11 line or axis of the fiber, reduces its value as the light  
12 beam reflects off the tapered surfaces. This reduction process  
13 is shown in greater detail in Fig. 5.

14  
15 In Fig. 5  $\theta_f$  is again the maximum angle which a light ray  
16 makes with the axis of the input fiber. However, when a  
17 reflection occurs at a point in the mixing rod in which tapering  
18 has already begun, and wherein the mixing rod has a radius  $R_1$   
19 and the tangent line at this point makes an angle  $\beta_1$  with  
20 respect to the center line of the fiber, the reflected light  
21 beam is rotated at an angle  $2\beta_1$ , so that it then makes an angle  
22  $(\theta_f - 2\beta_1)$  with respect to the central line of the fiber.  
23 Similarly, upon a second reflection at a point further along  
24 the mixing rod towards the output fiber, where the radius of  
25 the taper is  $R_2$ , the light beam is rotated by an additional  
26 angle  $2\beta_2$ , where  $\beta_2$  is the angle of the tangent line at radius  
27  $R_2$  with respect to the center line of the fiber. As a result,  
28 the light beam subsequent to this second reflection is at an  
29 angle with respect to the center line of the fiber that is equal  
30 to  $(\theta_f - 2\beta_1 - 2\beta_2)$ . It is evident that with multiple reflections  
31 along the edge of the tapered mixing rod, the angle of the

1 light beam is gradually reduced from the original angle  $\theta_f$ .  
2 Although in Fig. 5 the angles are exaggerated for purposes  
3 of discussion and clarity, the length of the mixing rod being  
4 considerably foreshortened in comparison to its diameter in  
5 Fig. 5, the reflective behavior of the light rays illustrated  
6 in Fig. 5 is representative of what actually occurs in the  
7 tapered mixing rod of the present invention.

8  
9 It will now be apparent that as a result of the reduction  
10 of the angle of the light ray with respect to the center  
11 line axis of the output fiber, the inherent random refractive  
12 bending due to surface imperfections at the output of the  
13 mixing rod, although still occurring, will not affect or will  
14 affect to a lesser degree the useable numerical aperture of  
15 the fiber optic transmission line in which the tapered mixing  
16 rod of the present invention is utilized in lieu of the  
17 straight mixing rod of the prior art. More briefly stated,  
18 the maximum bending due to such surface imperfections is less  
19 than the reduction of  $\theta_f$  provided by the tapered mixing rod.  
20 In other words,  $\theta_{f2}$  of Fig. 3 will usually be less than  $\theta_f$   
21 because of the prior reduction of  $\theta_f$  before the light ray  
22 exits the tapered mixing rod.

23  
24 An additional advantage of the tapered mixing rod as compared  
25 to the prior art straight mixing rod is that because the  
26 tapered rod diameter at the input end is substantially equal  
27 to the diameter of the input fiber, there is no need for a  
28 coupling junction corresponding to A1 in Fig. 2 for the prior  
29 art straight mixing rod configuration. As a result, there is  
30 an improvement in efficiency resulting from the obviation of  
31 the reflective and refractive losses that otherwise occur  
32 at such an input coupling point.

1     Fig. 6 represents a further refinement of the present  
2     invention in an embodiment suitable for coupler manufacture.  
3     As illustrated in Fig. 6, the tapered coupler 28 has been drawn  
4     or pulled into a single input fiber from 30. This pulling  
5     or drawing of the input fiber from the mixing rod itself,  
6     substantially eliminates losses at the input fiber/mixing rod  
7     interface. Additional coupling efficiency is provided by  
8     fusing the mixing rod to the output fiber group 34 at a fuse  
9     region FA shown in Fig. 6. The single, integral fiber/coupler  
10    configuration of Fig. 6 would typically include a cladding 32  
11    on the drawn fiber, however, this cladding would be present,  
12    inherently, if the mixing rod itself were also clad. In  
13    general, the mixing rod losses are minimized by using a fiber  
14    of as large a diameter as the mixing rod from which to draw  
15    the input fiber and taper the mixing rod geometry. Although  
16    the mixing rod geometry will be a function of the diameter  
17    and number of the input and output fibers to which the coupler  
18    assembly is designed to be mated, a typical 1 to 7 coupler  
19    mixing rod would have an input diameter of 5 mils, an output  
20    diameter of 20 mils and an overall length of 3 centimeters  
21    of which about 1 cm. is tapered. The mixing rod is usually  
22    fabricated of the same material as the fiber being coupled  
23    and may have either a graded index or step index cladding.

24  
25     It will now be apparent that what has been disclosed herein  
26     is a multi-port coupler for use in optical fiber transmission  
27     lines and which employs a unique mixing rod of novel tapered  
28     configuration to produce a highly advantageous improvement in  
29     light energy coupling efficiency. This improved efficiency  
30     results from a reduction in the number of coupling points and  
31     also from the retention of the inherent numerical aperture of  
32

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1 the coupled fibers despite random refractive bending that  
2 occurs due to imperfections in the surfaces of the coupler.  
3 Reduction of the maximum angle of light with respect to the  
4 center line axis of transmission in prior art couplers, does  
5 not occur in couplers utilizing the present invention because  
6 the tapered mixing rod provides gradual reflection angle  
7 reduction not provided by straight mixing rods of the prior art.  
8

9 Although a specific embodiment of the present invention has  
10 been disclosed, which embodiment represents the best mode  
11 contemplated by the inventors for practicing the invention,  
12 it will be apparent to those familiar with the art to which  
13 the invention pertains that various modifications and  
14 variations may be constructed without departing from the true  
15 spirit and scope of the invention. The scope of the invention  
16 being defined in the following claims:  
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CLAIMS

1. An improved apparatus for coupling light energy emanating from the port of at least one input optical transmission line to the respective ports of a plurality of output optical transmission lines, the improvement comprising:

an optical dispersion device intimately positioned between said input transmission line port and said output transmission ports,

said dispersion device having a first portion of cross-sectional area substantially equal to the cross-sectional area of said input transmission line port, having a second portion of cross-sectional area substantially equal to the combined cross-sectional area of said output transmission line ports, and having a third portion of gradually tapered cross section, integrally connecting said first portion to said second portion.

2. The improved coupling apparatus recited in Claim 1, wherein each of said optical transmission lines comprises a fiber optic cable.

3. The improved coupling apparatus recited in Claim 2, wherein said dispersion device is a mixing rod.

4. The improved coupling apparatus recited in Claim 3, wherein said input optical fiber cable is integrally connected to said first portion, having been formed by drawing said first portion into a longitudinally elongated extension thereof.

5. The improved coupling apparatus recited in Claim 4, wherein each of said output optical fibers is integrally connected to said mixing rod, each of said output optical fibers being fused to the third portion of said mixing rod.



6. In an apparatus for coupling light energy emanating from the port of at least one input optical transmission line to the respective ports of a plurality of output optical transmission lines and having an optical dispersion device intimately positioned therebetween, the input optical transmission line having a numerical aperture corresponding to a maximum angle,  $\theta_f$ , between the transmitted light and the longitudinal axis of the input optical transmission line; the improvement comprising:

means within said dispersion device for reducing the angle,  $\theta$ , between the transmitted light and the longitudinal axis of the dispersion device, for light entering said dispersion device at said angle  $\theta$  and reflecting, at least once, off the outer surface of said dispersion device, where  $\theta$  is defined as follows:

$$\theta \leq \theta_f.$$

7. The improved coupling apparatus recited in Claim 6, wherein each of said optical transmission lines comprises a fiber optic cable.

8. The improved coupling apparatus recited in Claim 7, wherein said dispersion device is a mixing rod.

9. The improved coupling apparatus recited in Claim 8, wherein said input optical fiber cable is integrally connected to said mixing rod having been formed by drawing from said mixing rod a longitudinally elongated extension thereof.

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10. The improved coupling apparatus recited in Claim 9, wherein each of said output optical fibers is integrally connected to said mixing rod, each of said output optical fibers being fused to said mixing rod at the end opposite said elongated extension.

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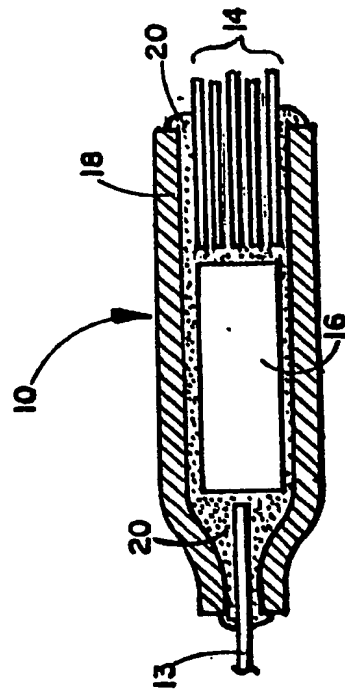


FIG. 1 (PRIOR ART)

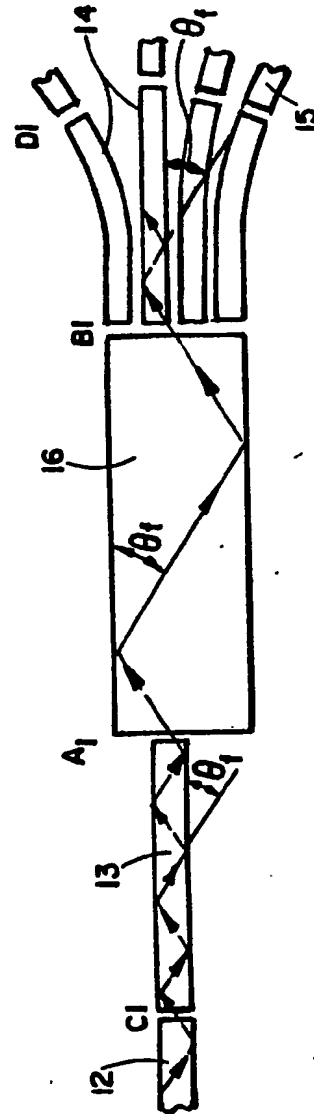


FIG. 2

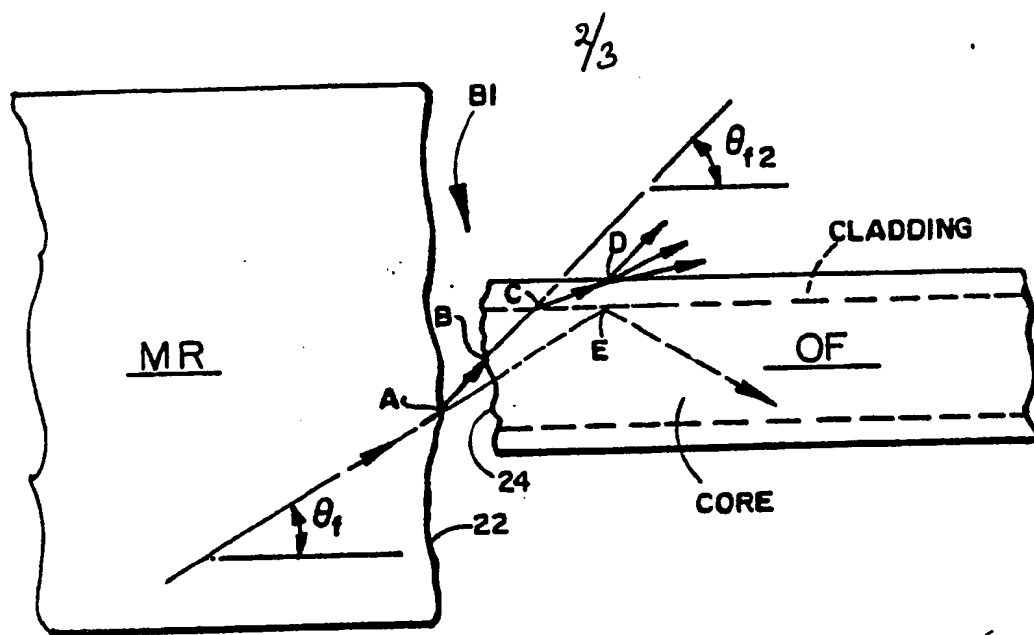


FIG. 3

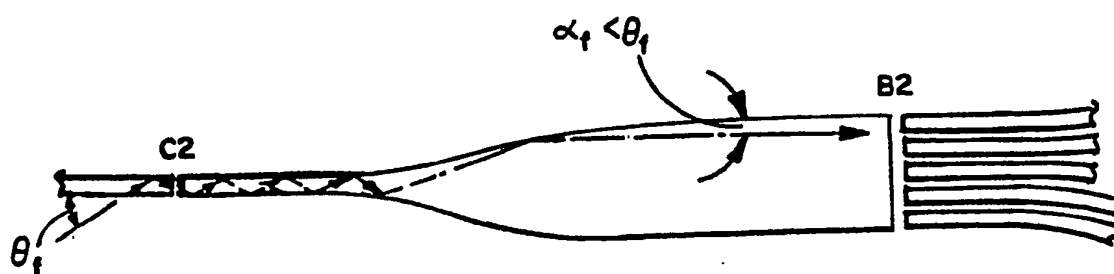
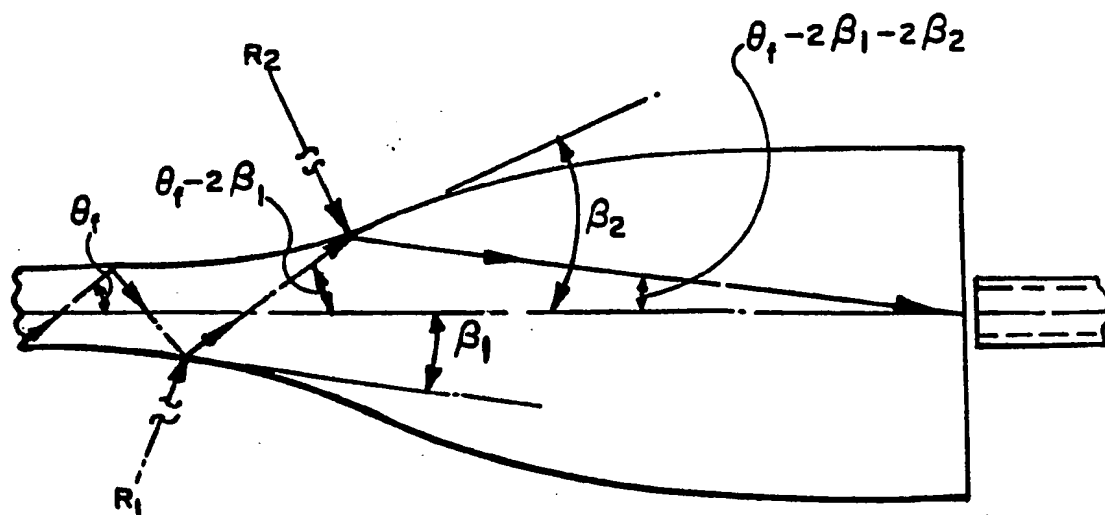
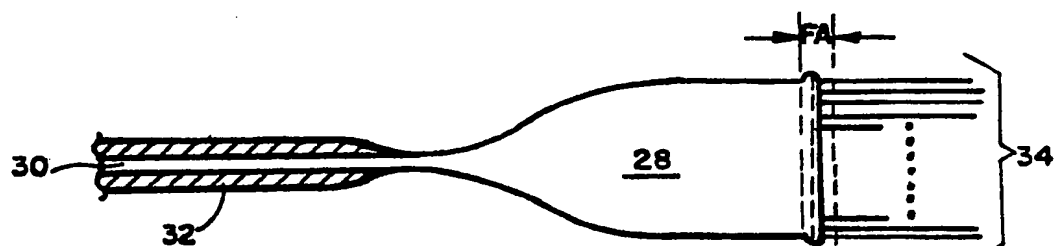


FIG. 4

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FIG. 5FIG. 6



## EUROPEAN SEARCH REPORT

EP 80 10 0310

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
X	<u>US - A - 3 901 581</u> (F.L. THIEL) * claims 1 and 2 *	1-8	G 02 B 5/14
	-- <u>US - A - 3 944 327</u> (H. LARSEN) * fig. 1 *	1	
	-- <u>US - A - 3 883 222</u> (L.C. GUNDERSON) * claim 4 *	1	
	-- <u>US - A - 3 779 628</u> (F.P. KAPRON et al.) * column 6, lines 1 to 4 *	9	TECHNICAL FIELDS SEARCHED (Int. Cl.)  G 02 B 5/14
A	-- <u>DE - A1 - 2 655 382</u> (SIEMENS AG) *claim 6 *	9	
A	-- <u>US - A - 3 832 028</u> (F.P. KAPRON) * fig. 2 *		
A	-- <u>US - A - 4 083 625</u> (M.C. HUDSON) * fig. 5 *		CATEGORY OF CITED DOCUMENTS X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons
A	-- <u>US - A - 3 610 755</u> (H. WIEBERGER et al.) * fig. 2 *		
	-- <u>US - A - 3 937 557</u> (A.F. MILTON) * fig. *		
			&: member of the same patent family, corresponding document
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
Berlin	28-04-1980	FUCHS	